



Inverse problems and machine learning in medical physics

Robotics in radiation therapy

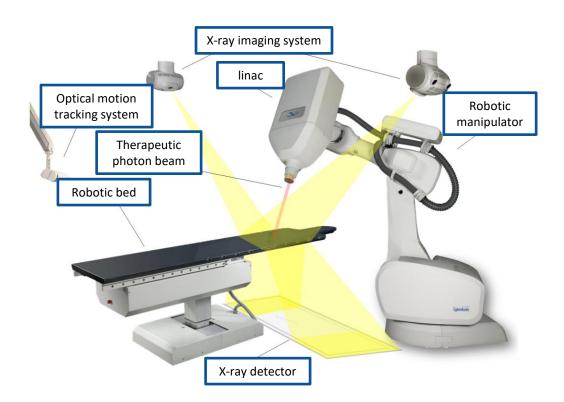
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The CyberKnife



- The CyberKnife is a radiation delivery system that features a linear accelerator (*linac*) directly mounted on a robot to deliver photons for radiation therapy, a fluoroscopic kV X-ray imaging for pre-treatment and intra-treatment image-guidance and an optical system for respiratory motion tracking
 - 3D conformal radiotherapy (3D-CRT), including intensity modulated radiation therapy (IMRT)
 - Stereotactic radiosurgery (SRS) and stereotactic body radiation therapy (SBRT) treatments



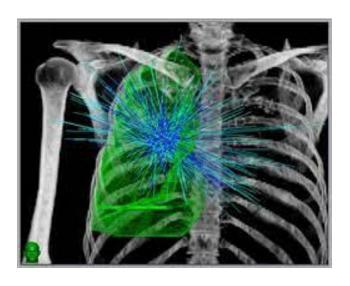


The CyberKnife



- The beams are delivered from fixed points in space called nodes, arranged in spherical (intracranial applications) or ellipsoidal (extracranial applications) configurations
- The combination of nodes and pointing vectors (twelve for each node) provides a set of "elementary beams" to plan the treatment





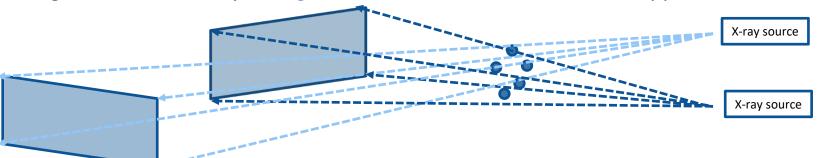


The CyberKnife



 Prior to the treatment, eight radiographic X-ray images in different breathing phases are compared to the DRRs of the treatment planning X-ray CT image to determine by triangulation the transformation to be applied to the 6-DoF robotic

bed for patient positioning



- During the treatment, this transformation is adjusted in real-time by moving the end-effector of the 6-DoF robotic manipulator (*linac*) according to the moving target
- The motion tracking considers:
 - Fiducial-free tumor tracking based on the optical tracking system (for external localization at 20–40 Hz) and implanted radio-opaque markers near or inside the tumor based on the X-ray imaging system (for internal localization every 30s) thus making use of external-internal correlation models
 - The model is constructed in ~30s at the beginning of the treatment and enables motion prediction for delay compensation (~ms)

 https://link.springer.com/content/pdf/10.1007%2F978-3-540-69886-9.pdf



LUDWIG-MAXIMILIANS-UNIVERSITÄT MÜNCHEN

The CyberKnife









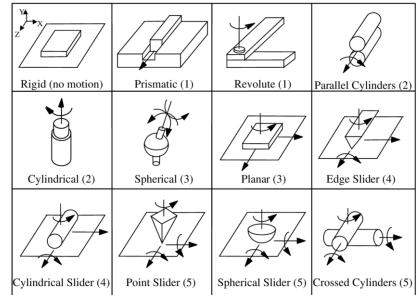
- First of all, we have to know where the robot is...
- Kinematics is the science of motion that treats motion without regard to the forces which cause it (i.e., position, velocity, acceleration...)

The forward kinematics problem is about the knowledge of the position of the end-effector, given the kinematic chain of

the mechanical system

 The kinematic chain is an assembly of links (rigid bodies) connected by joints providing degrees of freedom (DoF) to the end-effector

 the number of DoF of the end-effector is determined by the DoF of all the joints (i.e., 1-DoF for each revolute joint)

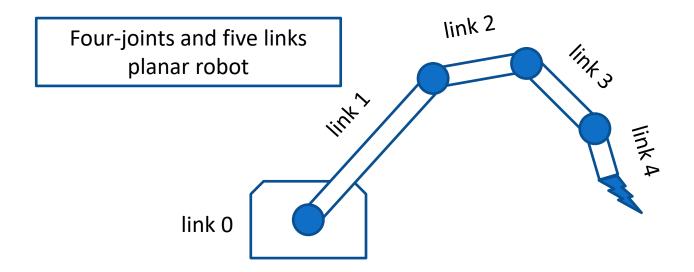


The kinematic chain is described by the joint variables (i.e., the angles for the revolute joints)





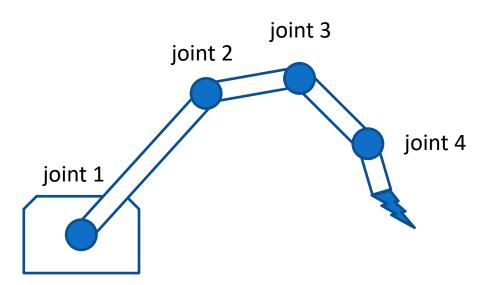
- In order to unequivocally localize the position of the end-effector in function of the angles of the kinematic chain (joints and links), the Denavit—Hartenberg convention (D-H convention) is commonly adopted
 - The n links are numbered from 0 (the base of the kinematic chain) to n-1 (the end-effector)







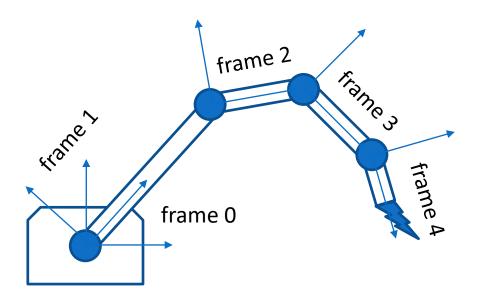
- In order to unequivocally localize the position of the end-effector in function of the angles of the kinematic chain (joints and links), the Denavit–Hartenberg convention (D-H convention) is commonly adopted
 - The n-1 joints are numbered from 1 to n-1 so that the joint n connects the link n-1 (the base of the kinematic chain) to the link n (the end-effector)







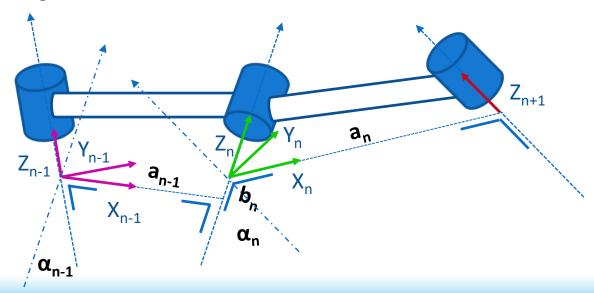
- In order to unequivocally localize the position of the end-effector in function of the angles of the kinematic chain (joints and links), the Denavit—Hartenberg convention (D-H convention) is commonly adopted
 - A frame n is defined at the joint n







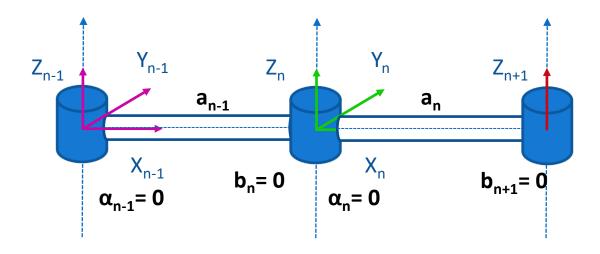
- Z_n is defined as the rotational axis of the revolute joint n
 - If Z_n and Z_{n+1} are skew lines, X_n is defined along the common perpendicular of Z_n and Z_{n+1} (the shortest distance between two skew lines is the distance between their intersection points with their common perpendicular), from Z_n to Z_{n+1}
 - The origin of the frame n is defined at the intersection point with Z_n
 - Y_n is defined according to the right-hand frame







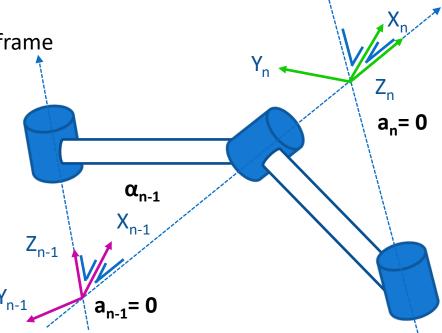
- Z_n is defined as the rotational axis of the revolute joint n
 - If Z_n and Z_{n+1} are parallel lines (i.e., planar robot), X_n is defined along the common normal of Z_n and Z_{n+1} , from Z_n to Z_{n+1}
 - The origin of the frame n is set on the joint n
 - Y_n is defined according to the right-hand frame







- Z_n is defined as the rotational axis of the revolute joint n
 - If Z_n and Z_{n+1} are intersecting lines, X_n is defined by the vector product between Z_n and Z_{n+1} (i.e., according to the righthand frame)
 - The origin of the frame n is set on the intersection point
 - Y_n is defined according to the right-hand frame





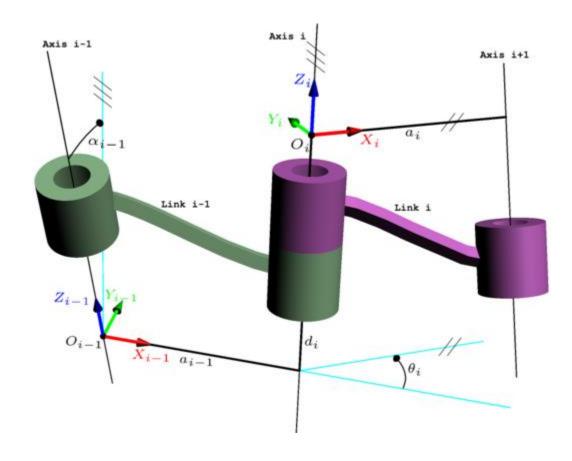


- Based on this convention, four Denavit—Hartenberg parameters (D-H parameters) are defined for each joint
 - I D-H parameter a_n (link length)
 - a_n is the absolute distance between Z_n and Z_{n+1}
 - II D-H parameter b_n (joint offset)
 - b_n is the distance along Z_n between X_{n-1} and X_n
 - III D-H parameter α_n (twist angle)
 - α_n is the angle between Z_n and Z_{n+1} across X_n (positive if counterclockwise)
 - IV D-H parameter ϑ_n (joint angle)
 - ϑ_n is the angle between X_{n-1} and X_n across Z_{n-1} (positive if counterclockwise)





Based on this convention, four Denavit—Hartenberg parameters (D-H parameters) are defined for each joint







 The forward kinematics describe the transformation of the frame n with respect to the frame n-1 as a composition of rotations and translations in the Denavit-Hartenberg matrix (D-H matrix)

$${}^{n-1}nT = R_X(\boldsymbol{\alpha}_{n-1})D_X(\boldsymbol{\alpha}_{n-1})R_Z(\boldsymbol{\vartheta}_n)D_Z(\boldsymbol{b}_n)$$

- Translation along Z_n equal to b_n
- Rotation across Z_n equal to ϑ_n
- Translation along X_{n-1} equal to a_{n-1}
- Rotation across X_{n-1} equal to α_{n-1}

$${}^{n-1}_{n}T = \begin{bmatrix} \cos(\boldsymbol{\vartheta}_{n}) & -\sin(\boldsymbol{\vartheta}_{n}) & 0 & \boldsymbol{\alpha}_{n-1} \\ \sin(\boldsymbol{\vartheta}_{n})\cos(\boldsymbol{\alpha}_{n-1}) & \cos(\boldsymbol{\vartheta}_{n})\cos(\boldsymbol{\alpha}_{n-1}) & -\sin(\boldsymbol{\alpha}_{n-1}) \\ \sin(\boldsymbol{\vartheta}_{n})\sin(\boldsymbol{\alpha}_{n-1}) & \cos(\boldsymbol{\vartheta}_{n})\sin(\boldsymbol{\alpha}_{n-1}) & \cos(\boldsymbol{\alpha}_{n-1}) \end{bmatrix} \begin{array}{c} \alpha_{n-1} \\ -\sin(\boldsymbol{\alpha}_{n-1})\boldsymbol{b}_{n} \\ \cos(\boldsymbol{\alpha}_{n-1})\boldsymbol{b}_{n} \end{bmatrix}$$

Rotation matrix ${n-1 \choose n}R$

Translation vector n-1 t





The forward kinematics describe the transformation of the end-effector frame with respect to the base frame (i.e., frame
 0) as a composition of D-H matrixes

$$e^{-0}T = {}^{0}_{1}T \dots {}^{n-1}_{e-e}T = \prod {}^{n-1}_{n}T = \begin{bmatrix} e^{-0}R & e^{-0}t\\ 0 & 0 & 1 \end{bmatrix}$$

- The position of the end-effector in the base frame (i.e., frame 0) ^{0}P is determined by the matrix-vector product of the composed D-H matrix with the position of the end-effector in the end-effector frame ^{e-e}P
 - The frame at the end-effector can be arbitrarily defined

$${}^{0}P = {}_{e} {}^{0}T^{e-e}P$$

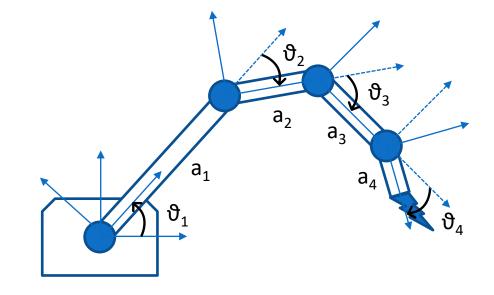
Descriptor of the forward kinematics





Four-joints and five links planar robot

Link	b _n	$\boldsymbol{\vartheta}_n$	a_n	α_n
1	0	$artheta_{\scriptscriptstyle 1}$	a ₁	0
2	0	ϑ_2	a_2	0
3	0	ϑ_3	a_3	0
4	0	$artheta_4$	a ₄	0



$${}_{4}^{0}T = {}_{1}^{0}T {}_{2}^{1}T {}_{3}^{2}T {}_{4}^{3}T$$

$${}_{4}^{0}T = \begin{bmatrix} \cos(\boldsymbol{\theta_{1}}) & -\sin(\boldsymbol{\theta_{1}}) & 0 & 0 \\ \sin(\boldsymbol{\theta_{1}}) & \cos(\boldsymbol{\theta_{1}}) & 0 & 0 \\ 0 & 0 & 1 & 0 \\ 0 & 0 & 0 & 1 \end{bmatrix} \begin{bmatrix} \cos(\boldsymbol{\theta_{2}}) & -\sin(\boldsymbol{\theta_{2}}) & 0 & a_{1} \\ \sin(\boldsymbol{\theta_{2}}) & \cos(\boldsymbol{\theta_{2}}) & 0 & 0 \\ 0 & 0 & 1 & 0 \\ 0 & 0 & 0 & 1 \end{bmatrix} \begin{bmatrix} \cos(\boldsymbol{\theta_{3}}) & -\sin(\boldsymbol{\theta_{3}}) & 0 & a_{2} \\ \sin(\boldsymbol{\theta_{3}}) & \cos(\boldsymbol{\theta_{3}}) & 0 & 0 \\ 0 & 0 & 1 & 0 \\ 0 & 0 & 0 & 1 \end{bmatrix} \begin{bmatrix} \cos(\boldsymbol{\theta_{4}}) & -\sin(\boldsymbol{\theta_{4}}) & 0 & a_{3} \\ \sin(\boldsymbol{\theta_{4}}) & \cos(\boldsymbol{\theta_{4}}) & 0 & 0 \\ 0 & 0 & 1 & 0 \\ 0 & 0 & 0 & 1 \end{bmatrix}$$



The "inverse" kinematics



- Finally, we have to know where the robot goes...
- The inverse kinematics problem is about the knowledge of the kinematic chain of the mechanical system, given the desired
 position of the end-effector (i.e., the task)
- The solution of the inverse kinematics problem is defined within the workspace of the mechanical system
 - If the task is outside the workspace, the solution does not exist
 - If the solution exists, this can be single or multiple (infinite) depending on the DoF of the mechanical system



The "inverse" kinematics



- The number of unknowns is defined by the DoF of the joints of the mechanical system
- The forward kinematics given by $e^{-0}e^T$ provide 16 equations but 4 of them are trivial. Among the remaining 12 equations, 3 equations are relevant to the position-vector $e^{-0}e^t$ and 9 equations are relevant the rotation-matrix $e^{-0}e^t$. In the rotation-matrix only 3 equations are independent. The number of equations is therefore 6.
- The kinematic equations are nonlinear and transcendental, their solution is not always easy (or even possible) in a closedform
 - For a 6-DoF robot, there are 6 equations and 6 unknowns. In this case, the analytical solution of the inverse kinematic problem is feasible





The "inverse" kinematics



- Numerical methods (i.e., iterative optimization algorithm) based on approximation and derivatives of the forward-kinematics function for finding the local minimum
- If n the number of joint variables, the forward-kinematics function maps a point in the joint space to an end-effector position in the workspace

$$p(x): \mathbb{R}^n \to \mathbb{R}^3$$

- Given the initial position of the system $p_0 = p(x_0)$, the task is defined as $p_1 = p(x_0 + \Delta x)$
- Given the Jacobian of the forward-kinematics function $J_p(x_0)$, whose size is 6 x n, the Taylor series expansion of the forward-kinematics function, valid for small Δx , is calculated as:

$$p(x_1) \approx p(x_0) + J_p(x_0) \Delta x$$

By calculating the (pseudo) inverse $J_p^{inv}\left(x_0\right)$, the updating step is defined as:

$$\Delta x \approx J_p^{inv}(x_0)\Delta p(x_0)$$
 with $\Delta p = p(x_0 + \Delta x) - p(x_0)$, and thus $\Delta x_{k+1} \approx J_p^{inv}(x_k)\Delta p_k$



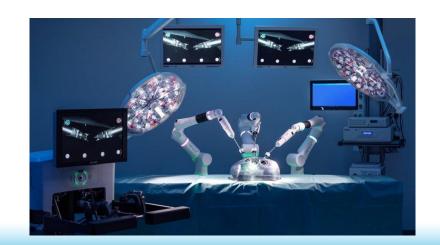


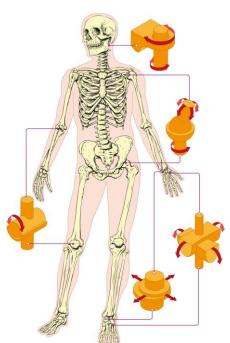
Robotics and artificial intelligence

- The human body is a mechanical system made of joints and links that can implement a task
- The human senses define the control system that can provide information about the task
- The human brain is the intelligence system that can decide the task based on the sensor information



artificial intelligence-driven robots





Robotic surgery



Robotics and artificial intelligence



- In radiation oncology, the task is executed based on the patient model in the treatment planning scenario
- The task is adapted based on imaging and sensor systems for monitoring the treatment delivery scenario, thus adapting the *real* patient to the patient model (i.e., patient positioning) or vice versa, to adapt the patient model to the *real* patient (i.e., treatment adaptation and tumor tracking)
 - Correction models are defined (i.e., anatomical correction models, external-internal correlation models)
 - Model-free adaptive tasks based on Al

